



DEPARTMENT OF THE NAVY  
MARE ISLAND NAVAL SHIPYARD  
VALLEJO, CALIFORNIA 94592

N00221\_000109  
MARE ISLAND  
SSIC NO. 5090.3.A

IN REPLY REFER TO:

5090  
Ser 461.6/109

APR 1 1988

Ms. Lila Tang  
San Francisco Bay Region  
California Regional Water  
Quality Control Board  
1111 Jackson Street  
Oakland, CA 94607

Dear Ms. Tang:

Pursuant to the California Regional Water Quality Control Board order No. 87-170, paragraph C.3.b., Mare Island Naval Shipyard has prepared an investigation of the minimum freeboard requirement for the Industrial Wastewater Treatment Plant surface impoundments.

The investigation showed that the 18 inch freeboard in the blending ponds is adequate for the containment of the maximum probable precipitation, the tidal and wave action generated by the maximum recorded wind for the last ten years.

Attached is a copy of the study and the calculations in support of the above conclusion. Any questions on these topics can be directed to Mr. Tony Lee, Environmental Engineer, Code 461.6, telephone number (707) 646-3375.

Sincerely,

W. J. CORNILS  
Head, Environmental-Energy  
Management Division  
By direction of the Shipyard Commander

Enclosure

Copy to:  
United States Environmental Protection Agency  
Region IX  
Toxics and Waste Management Division, Code M-5  
215 Fremont Street  
San Francisco, CA 94105  
Attention: Ms. Karen Scheuermann

California Department of Health Services  
North Coast California Section  
Toxic Substances Control Division  
5850 Shellmound Drive, Suite 390  
Emeryville, CA 94608  
Attention: Mr. John O'Kane

Solano County Department of Public Health  
601 Texas Street  
Fairfield, CA 94533  
Attention: Cliff Covey

Commander  
Western Division, Naval Facilities  
Engineering Command  
Code 1142  
P. O. Box 727  
San Bruno, CA 94066  
Attention: Mr. Dean Peterson

CALCULATIONS

3-16-88

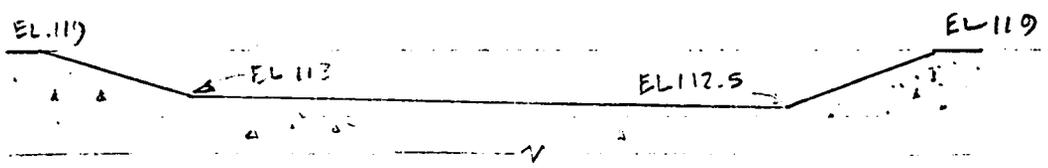
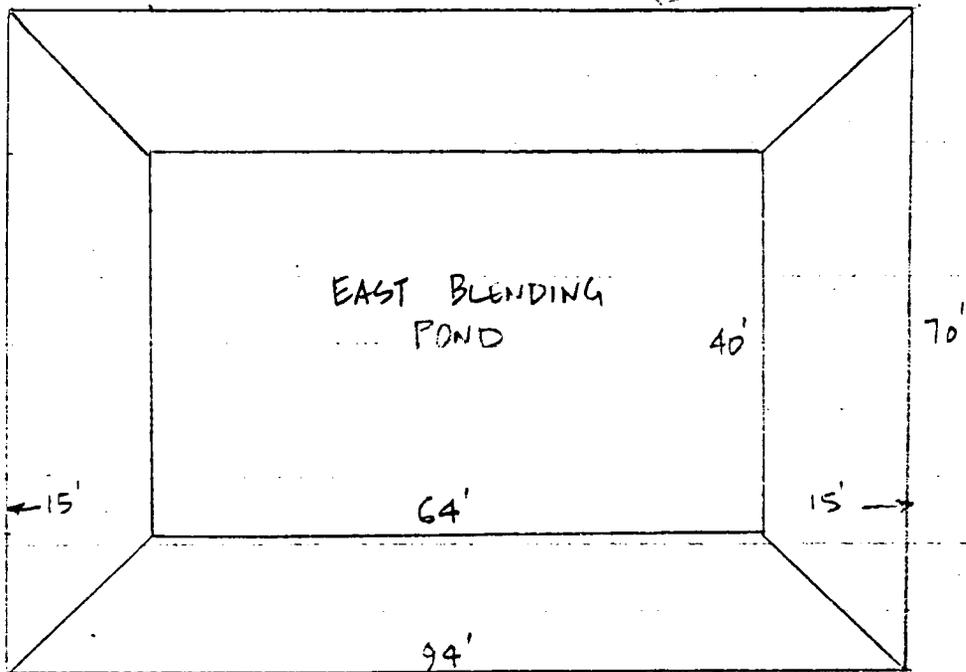
AKL

OBJ = EST. THE FREEBOARD FRLM FOR THE WTP EAST BLENDING POND

- METHOD 1) CHECK FREEBOARD CAPACITY FOR HOLDING THE MAX. PROBABLE PRECIP (TABLE 4.1, 33 CAC 2541) ; CLASS I WASTE MGMT. UNIT
- 2) IN ADDITION, CHECK WAVE HEIGHTS & WIND TIDES BASED ON WIND GENERATED WAVE & TIDE ACTIONS

BASIS: 1) MAX WIND SPEED = 60 KNOTS  
 (BASED ON WIND SPEED WESTERLY DIRECTION MEASUREMENTS FROM 1981 TO 1985)  $\approx$  69 MILES/HR

2) POND DIMENSIONS



3-16-88

AMM

1) EST. FREEBOARD CAPACITY OF POND

$$\begin{aligned}
 &\rightarrow \text{CAPACITY IF POND IS FILLED TO HIGHEST POINT (EL. 115)} \\
 &= \text{VOL. OF SLOPED SECTION} + \text{VOL. OF FLAT SECTION} \\
 &= (15' \times 6' \times 55') + (15' \times 6.5' \times 55') + (40' \times 64') \frac{6.5' + 6'}{2} \\
 &= 4950 \text{ FT}^3 + 5362 \text{ FT}^3 + 16,000 \text{ FT}^3 \\
 &= 26,312 \text{ FT}^3 = \underline{\underline{196,810 \text{ GALLONS}}}
 \end{aligned}$$

PART B. APPLICATION SHOWS 206,600 GALLONS  
CLOSE ENOUGH 2.5% DIFF.

$$\begin{aligned}
 &\rightarrow \text{CAPACITY IF POND IS FILLED TO CURRENT FREEBOARD LEVEL} \\
 &\quad (\text{EL. 117.5}) \\
 &= (15' \times 4.5' \times 55') + (15' \times 5' \times 55') + (40' \times 64') \frac{4.5' + 5'}{2} \\
 &= (3713 + 4125 + 12,160) \text{ FT}^3 \\
 &= 19,998 \text{ FT}^3 = \underline{\underline{149,580 \text{ GALLONS}}}
 \end{aligned}$$

$$\begin{aligned}
 &\rightarrow \text{CAPACITY ABOVE FREEBOARD LEVEL} \\
 &= 196,810 - 149,580 = \underline{\underline{47,230 \text{ GALLONS}}}
 \end{aligned}$$

3-16-88 AKL

THE MAXIMUM PROBABLE PRECIPITATION IN THE MINDY AREA IS A 100-YEAR, 24-HR DURATION STORM WITH RAINFALL OF 4.99 INCHES (BASED ON 105 YEARS OF RAINFALL RECORD, TABLE 5-1, HYDROLOGY AND DRAINAGE DESIGN PROCEDURE, COUNTY OF SOLANO, OCT. 1977)

THE VOLUME OF RAINFALL OVER THE POND AREA IS

$$\left( \frac{4.99}{12} \times 70' \times 94' \right) = 2736 \text{ FT}^3 = \underline{\underline{20,470 \text{ GALLONS}}}$$

2. THE VOLUME ABOVE THE FREEBOARD HAS APPROX. 2.3 TIMES THE NEEDED CAPACITY.

2) ESTIMATE WIND GENERATED WAVE

FROM THE "STANDARD HANDBOOK FOR CIVIL ENGINEERS",  
 FEDERICK S. MERRIT, EDITOR, 1968, MCGRAW HILL.  
 EQUATION 23-11 p. 23-7

WAVE HEIGHT IS RELATED TO WIND VELOCITY & FETCH AS FOLLOWS

$$H = 0.0555 U F^{0.5}$$

H = SIGNIFICANT WAVE HT, FT

U = WIND VELOCITY, KNOTS

$$H = 0.0555 (60 \text{ KNOTS}) \left( \frac{94 \text{ FT. MILE}}{5280 \text{ FT (1.15)}} \right)^{0.5} \quad F = \text{FETCH, NAUTICAL MILES}$$

$$= 0.414 \text{ FT} = \underline{\underline{5 \text{ INCHES}}}$$

3) EXT. WIND TIDES

FROM THE "HANDBOOK OF HYDRAULICS" BY KING & BRATER, 5TH ED.  
 EQU. 10-87 & 10-88 DEVELOPED BY SIBUL:

$$\frac{h}{d} = 2.44 \times 10^{-5} \left( \frac{F}{d} \right)^{1.66} \left( \frac{U^2}{Fg} \right)^2 \quad (\text{EQU 10-87})$$

$$z = 2.02 \left( \frac{F}{d} \right)^{-0.0768} \quad (\text{EQU 10-88})$$

WHERE  $h$  = INCREASE IN DEPTH OF  
 WATER DUE TO WIND, FT.

$d$  = DEPTH OF WATER, FT = 5 FT

$F$  = WIND FETCH, FT = 94 FT

$U$  = WIND SPEED, MILES/HR = 69 MPH

$g$  = GRAVITATIONAL ACCELERATION

FT/SEC<sup>2</sup> = 32.2 FT/SEC<sup>2</sup>

$$z = 2.02 \left( \frac{94}{5} \right)^{-0.0768}$$

$$= 1.612$$

$$\frac{h}{5} = 2.44 \times 10^{-5} \left( \frac{94}{5} \right)^{1.66} \left[ \frac{(69 \frac{\text{miles}}{\text{HR}}) \left( \frac{5200 \text{ FT}}{\text{mile}} \right) \left( \frac{\text{HR}}{3600 \text{ SEC}} \right)}{94 (32.2)} \right]^2 = 6.796$$

$$h = 0.11 \text{ FT} = \underline{\underline{1.3''}}$$

WIND VELOCITY DATA FOR 1976 - 1986  
AT MAKE ISLAND NAVAL SHIPYARD

⇒ MAX WIND VELOCITY IN THIS PERIOD

= 60 KNOTS (112.2)

~ 69 MPH

1966

ELEVATION - ~ 90'

	<u>MAX. WIND VELOCITY (KNOTS)</u>	<u>DIRECTION</u>
JAN	NO DATA	-
FEB	⇒ 42	WSW
MAR.	36	NW
APR.	22	S, NW, NNW
MAY	23	WNW
JUN	24	NNE
JULY	21	S
AUG	20	WSW
SEPT	24	WNW
OCT	NO DATA	-
NOV.	NO DATA	-
DEC	NO DATA	-

1935

ELEVATION - 10.5 FT. QUAY WALL

MAX WIND VELOCITIES (KNOTS)DIRECTION

JAN.	⇒	55	E
FEB		35	ENE
MAR		45	ENE
APR		24	N, WSW
MAY		24	SSW, SW
JUN		22	SSE
JULY		22	WSW, WNW
AUG		23	W
SEPT.		22	W, WNW
OCT.		20	SSE
NOV.		19	W, WSW
DEC		16	W

1964

ELEVATION - ~ 90'

	<u>MAX. WIND VELOCITY (MPH)</u>	<u>DIRECTION</u>
JAN	30	ENE
FEB	30	SSW
MAR	25	WNW
APR	29	W
MAY	35	N
JUN	⇒ 50	SSW
JULY	NO DATA	-
AUG.	22	SSE, SSW
SEPT.	27	NW
OCT.	24	NNW
NOV.	25	S, SSE
DEC	25	E

1973

ELEVATION - ~ 90'

MAX. WIND VELOCITY (KNOTS)DIRECTION

JAN	25	E
FEB	30	S
MAR	24	W, S
APR	23	NNW
MAY	30	N, NNE
JUN	24	SSW
JULY	23	E
AUG	22	S
SEPT.	18	W
OCT.	18	ENE, WSW
NOV.	⇒ 35	SSE
DEC.	⇒ 35	W, WNW

1982

ELEVATION - ~ 90'

MAX WIND VELOCITY (KNOTS)

DIRECTION

		<u>MAX WIND VELOCITY (KNOTS)</u>	<u>DIRECTION</u>	
JAN		24	ESE	
FEB	⇒	60	6%	N
MAR		25	SSW, SW, WSW	
APR		30	WSW	
MAY		23	WSW	
JUN		NO DATA		
JULY	⇒	60	W	
AUG		21	WNW, NNW	
SEPT		23	N	
OCT		20	W	
NOV.		35	W, S	
DEC		23	S	

1181

ELEVATION - ~ 90'

MAX. WIND VELOCITY (KNOTS)

DIRECTION

JAN	27	E
FEB	21	W
MAR	35	WSW
APR	22	W
MAY	30	W
JUN	23	W
JULY	24	S
AUG	20	S, WSW, W
SEPT.	21	S, WSW
OCT.	37	WNW
NOV.	⇒ 50	S
DEC.	27	E

1980

MONTH	MAR. WIND SPEED (KNOTS)	DIRECTION
JAN	23	N
FEB	25	NNE
MAR	25	N, NNE, W
APR	24	S, WNW, NW, NNW
MAY	⇒ 56	ENE
JUN	24	SSW
JULY	22	SSW, W
AUG	22	WSW
SEPT	17	S, SSW
OCT.	17	W
NOV.	23	ESE
DEC	24	ESE, SSE

TYPE OF OBSERVATION: HOURLY  
TOTAL OBSERVATIONS = 7960

\*\*\*\*\*  
\* METEOROLOGICAL RECORDS FOR THE PERIOD \*  
\* BEGINNING 1/ 1/79 \*  
\* ENDING 12/31/79 \*  
\*\*\*\*\*

LATITUDE: 28 25' 55.13"  
LONGITUDE: 122 16' 32.13"

FOR THE YEAR OF 1979

\*\*\* WIND DATA \*\*\*

\*\*\* TEMPERATURE (FAHRENHEIT) \*\*\*

DIRECTION	VELOCITY (KNOTS)		FREQUENCY BY		MAXIMUM	MINIMUM	AVERAGE	NO. READINGS
	MAXIMUM	AVERAGE	NUMBER	PERCENT	102.	35.	63.1	7960
N	30.	4.4	1083	13.6	*** HUMIDITY (PERCENT) ***			
NNE	15.	3.3	53	0.7	MAXIMUM MINIMUM AVERAGE NO. READINGS			
NE	15.	6.4	45	0.6	98.	28.	73.6	7960
ENE	16.	4.6	121	1.5	*** BAROMETRIC PRESSURE (INCH HG) ***			
E	18.	5.5	547	6.9	MAXIMUM MINIMUM AVERAGE NO. READINGS			
ESE	22.	6.5	302	3.8	30.99	28.95	30.16	7960
SE	17.	6.8	138	1.7	*** WEATHER CONDITIONS (PERCENT) ***			
SSE	21.	5.3	169	2.1	CLEAR PARTLY CLOUDY CLOUDY NO. READINGS			
S	22.	6.4	551	6.9	54.4	22.0	23.7	7643
SSW	22.	8.9	834	10.5	CALM WIND			
SW	23.	8.4	794	10.0	NUMBER PERCENT			
WSW	24.	8.6	1447	18.2	266	3.3		
W	24.	8.7	1407	17.7	END OF FILE 9999			
WNW	17.	5.2	264	3.3				
NW	18.	4.8	72	0.9				
NNW	23.	5.9	133	1.7				

1978

MONTH	MAX. WIND SPEED (KNOTS)	DIRECTION
JAN	22	N, S, SSW, SW
FEB	16	WNW
MAR	21	S, SSW, SW, W
APR	22	WSW
MAY	NA	-
JUN	21	WSW, W, WNW
JULY	NA	-
AUG	⇒ 24	S
SEPT.	⇒ 24	S, W
OCT.	NA	-
NOV	18	N, NW
DEC	NA	-

TYPE OF OBSERVATION: HOURLY  
 TOTAL OBSERVATIONS = 7056

\*\*\*\*\*  
 \* METEOROLOGICAL RECORDS FOR THE PERIOD \*  
 \* BEGINNING 1/ 1/77 \*  
 \* ENDING 12/31/77 \*  
 \*\*\*\*\*

LATITUDE: 28 25' 55.13"  
 LONGITUDE: 122 16' 32.13"

FOR THE YEAR OF 1977

\*\*\* WIND DATA \*\*\*

\*\*\* TEMPERATURE (FAHRENHEIT) \*\*\*

DIRECTION	VELOCITY (KNOTS)		FREQUENCY		MAXIMUM	MINIMUM	AVERAGE	NO. READINGS
	MAXIMUM	AVERAGE	NUMBER	PERCENT				
					102.	39.	64.0	7056
N	20.	4.6	240	3.4				
NNE	18.	6.5	55	0.8				
NE	18.	3.6	161	2.3				
ENE	13.	5.5	68	1.0				
E	21.	6.6	395	5.6				
ESE	19.	6.4	246	3.5				
SE	16.	5.0	498	7.1	97.	20.	69.8	7056
SSE	18.	5.4	49	0.7				
S	24.	6.0	174	2.5				
SSW	21.	6.9	171	2.4				
SW	25.	8.0	774	11.0				
→ WSW	46.	8.4	1568	22.2				
W	23.	7.0	1329	18.8	30.98	27.00	30.22	7056
WNW	23.	6.6	806	11.4				
NW	20.	5.2	424	6.0				
NNW	17.	4.8	98	1.4				

\*\*\* HUMIDITY (PERCENT) \*\*\*

MAXIMUM	MINIMUM	AVERAGE	NO. READINGS
97.	20.	69.8	7056

\*\*\* BAROMETRIC PRESSURE (INCH HG) \*\*\*

MAXIMUM	MINIMUM	AVERAGE	NO. READINGS
30.98	27.00	30.22	7056

\*\*\* WEATHER CONDITIONS \*\*\*  
(PERCENT)

CLEAR	PARTLY CLOUDY	CLOUDY	NO. READINGS
71.8	15.4	12.8	6311

CALM WIND

NUMBER	PERCENT
260	3.7

END OF FILE 9999

TYPE OF OBSERVATION: HOURLY  
 TOTAL OBSERVATIONS = 8577

\*\*\*\*\*  
 \* METEOROLOGICAL RECORDS FOR THE PERIOD \*  
 \* BEGINNING 1/ 1/76 \*  
 \* ENDING 12/31/76 \*  
 \*\*\*\*\*

LATITUDE: 28 25' 55.13"  
 LONGITUDE: 122 16' 32.13"

FOR THE YEAR OF 1976

\*\*\* WIND DATA \*\*\*

\*\*\* TEMPERATURE (FAHRENHEIT) \*\*\*

DIRECTION	VELOCITY (KNOTS)		FREQUENCY BY		MAXIMUM	MINIMUM	AVERAGE	NO. READINGS
	MAXIMUM	AVERAGE	NUMBER	PERCENT				
					105.	5.	64.8	8577
N	24.	3.8	229	2.7				
NNE	19.	4.5	99	1.2				
NE	22.	2.2	403	4.7				
ENE	18.	4.5	68	0.8				
E	25.	4.8	391	4.6				
ESE	16.	5.3	274	3.2				
SE	18.	3.9	685	8.0	100.	17.	70.3	8577
SSE	12.	3.3	80	0.9				
S	16.	2.8	145	1.7				
SSW	20.	5.0	78	0.9				
SW	22.	6.9	880	10.3				
WSW	27.	7.8	2081	24.3				
W	22.	6.4	1421	16.6				
WNW	20.	6.2	1220	14.2	31.42	29.00	30.24	8577
N /	20.	4.4	478	5.6				
NNW	11.	3.3	51	0.6				

\*\*\* HUMIDITY (PERCENT) \*\*\*

MAXIMUM MINIMUM AVERAGE NO. READINGS

100. 17. 70.3 8577

\*\*\* BAROMETRIC PRESSURE (INCH HG) \*\*\*

MAXIMUM MINIMUM AVERAGE NO. READINGS

31.42 29.00 30.24 8577

\*\*\* WEATHER CONDITIONS \*\*\*  
 (PERCENT)

CLEAR PARTLY CLOUDY CLOUDY NO. READINGS

71.4 15.6 13.0 7971

CALM WIND

NUMBER PERCENT

653 7.6

## FREEBOARD

### IWTP SURFACE IMPOUNDMENTS FREEBOARD REQUIREMENTS STUDY

#### BACKGROUND

California Regional Water Quality Control Board (RWQCB) order no. 87-170 of December 21, 1987 requires MINS to comply with section 2548 of subchapter 15 of Title 23 CAC, or demonstrate that a minimum freeboard of less than 2 feet is adequate to prevent overtopping of the IWTP surface impoundments. Section 2548a of subchapter 15 of Title 23 CAC required that surface impoundments shall have sufficient freeboard to accomodate seasonal precipitation and precipitation conditions specified for each class of waste management unit in table 4.1 of the same article, but in no case less than 2 feet and shall be designed and constructed to prevent overtopping as a result of wind conditions likely to accompany such precipitation conditions. The IWTP surface impoundments are considered by the RWQCB for the purpose of the waste discharge requirements to be class I waste management units and as such they must be designed for maximum probable precipitation.

#### METHODOLOGY

The present IWTP surface impoundments are operated with an 18-inch freeboard in the blending ponds. The adequacy of the 18-inch freeboard will be investigated base on the following probable conditions:

- o Increased capacity requirement due to rainfall from a maximum probable precipitation;
- o Increased liquid height due to wave action generated by the maximum recorded wind speed (wind speed data from 1976 to 1986);
- o Increased liquid height due to tidal action generated by the maximum recorded wind speed (wind speed data from 1976 to 1986).

Overtopping of the blending pond containment will be investigated for all three conditions.

#### STUDY RESULTS

(see attached calculations for details)

##### CASE 1 - MAXIMUM PROBABLE PRECIPITATION

The estimated volume available in the 18-inch freeboard section of the ponds is 47,200 gallons. The maximum probable precipitation volume based on a 24-hr 100 year storm is 20,500 gallons. Therefore each blending pond has more than twice the required volume to handle the maximum probable precipitaion.

##### CASE 2 - WAVE ACTION GENERATED BY THE MAXIMUM RECORDED WIND SPEED

The maximum recorded wind speed for the period from 1976 to 1986 is 60 knots (69 miles per hour). Based on this speed and equation 23 - 11 for wind generated wave, (from the Standard Handbook for Civil Engineers, Frederick S. Merrit, Editor) the wave height is estimated to be 5 inches. This is still within the 18-inch operating freeboard of the blending ponds.

### CASE 3 - TIDAL ACTION GENERATED BY THE MAXIMUM RECORDED WIND SPEED

The maximum recorded wind speed for the period from 1976 to 1986 is 60 knots (69 miles per hour). Based on this speed and the Sibul correlation for wind generated tidal action, the estimated increase in the still liquid height is 1.3 inches. This will not present any overtopping problem with the 18-inch operating freeboard of the blending ponds.

### CONCLUSIONS

The IWTP blending ponds with the current 18-inch operating freeboard will have no problem accomodating the maximum probable precipitaion or the windtide and wind wave generated by the maximum recorded wind speed for the years 1976 to 1986.